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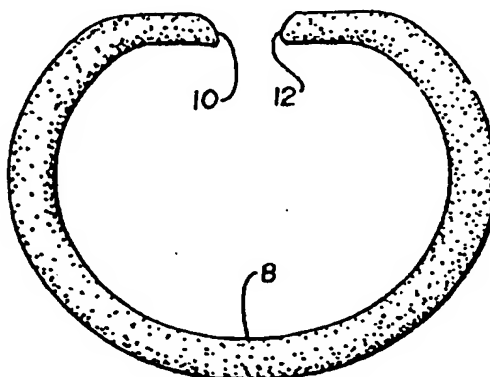
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(54) Title: BIORESORBABLE ANNULOPLASTY PROSTHESIS

(57) Abstract

This invention relates to heart valve annuloplasty prostheses that are fashioned of bioresorbable materials. The prostheses are eventually resorbed by the patient, during which time regenerated tissue replaces the prosthesis. This leaves the patient with a biological and functional annular structure, resulting in improved heart valve function.



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## BIORESORBABLE ANNULOPLASTY PROSTHESIS

Field of the Invention

This invention relates to biocompatible annuloplasty prostheses that are resorbed by the patient  
5 following implantation.

Background of the Invention

Human heart valves comprise leaflets or cusps that open and close to control the flow of blood to a particular region of the heart. The mitral and tricuspid  
10 valves are located in the atrioventricular opening of the heart and function to prevent backflow of blood from the ventricle into the atrium when the ventricle contracts. The aortic valve is located between the left ventricle and the ascending aorta and functions to prevent backflow  
15 of blood into the left ventricle.

The mitral valve is located in the left atrioventricular opening of the heart. It includes two leaflets or cusps and is encircled by a dense fibrous ring known as the annulus. The anterior leaflet is  
20 located next to the aortic valve and is also known as the anterior medial leaflet. The posterior leaflet has a wider attachment to the annulus and is also known as the posterior lateral leaflet. The leaflets are held in place by chordae tendineae and papillary muscles. The  
25 commissure is the point at which the annular attachment of the leaflets meet and fuse. Coaptation refers to

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valve closure and the meeting of the free edges of the leaflets.

The tricuspid valve is located in the right atrioventricular opening and comprises three leaflets, sometimes referred to as the anterior, posterior and septal cusps (leaflets). These leaflets are roughly triangular in shape and, like the mitral valve leaflets, are attached to a fibrous ring, or annulus.

The aortic valve is composed of three segments, each of which is termed a semilunar cusp. The valve is closed during ventricular diastole and is open during systole.

The most common defect leading to mitral dysfunction is a dilation or elongation of the posterior two-thirds of the annulus, the section corresponding to the posterior leaflet. The anterior section of the annulus is anchored to the aortic root and is therefore not as subject to elongation. However, not infrequently in cases of mitral valve dysfunction, the anterior leaflet is displaced away from the center of the valve and is slightly thickened and shortened. Thus, in repairing a mitral valve, it is sometimes necessary to reduce the annulus to its physiological dimensions by repairing the dilated portion of the valve, to ensure coaptation. It may also be necessary to restore the commissure to its normal curvature and to reposition and

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reshape the anterior leaflet. Similar concepts apply to correction of tricuspid valve defects.

Mitral valve repair has been performed successfully since the late 1950's. Its appeal with 5 cardiac surgeons, however, was not immediate. Only in more recent years, as surgeons have had appropriate devices to use and have increasingly realized the advantages of repair, has the proportion of mitral valves repaired increased. The clinical advantages of mitral 10 valve repair as compared to replacement are attributed to better left ventricular function and the lack of need for long-term anticoagulation therapy. Better left ventricular function has led to a lower incidence of mitral valve stenosis and regurgitation for repair as 15 compared to replacement procedures. The incidences of thromboembolism, hemorrhagic complications and infective endocarditis have been shown to be lower after mitral valve repair than after replacement. Actuarial survival after repair is also greater than that after valve 20 replacement. Akins et al., Ann. Thorac. Surgery 58: 668-76 (1994).

Annuloplasty, or annulus repair, has become an intermediate measure between non-invasive management of valvular heart disease and replacement of an entire heart 25 valve with a prosthetic implant. Annuloplasty prostheses, for example ring-shaped devices, are used in

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the procedures and represent the standard method of repair. As clinical results increasingly show that annuloplasty prostheses better preserve left ventricular function, surgeons have become more enthusiastic about  
5 annuloplasty repair over valve replacement whenever feasible.

Annuloplasty prostheses differ from prosthetic heart valves in that the prostheses are designed to support diseased or damaged natural heart valves rather  
10 than replace them. An annuloplasty prosthesis is a device implanted around or in association with the mitral, tricuspid or aortic valve for reconstructive repair of valvular insufficiency. The indications for repair using annuloplasty prostheses include correction  
15 of annular dilatation, increases in leaflet coaptation, reinforcement of annular suture lines and prevention of future dilatation. Annuloplasty prostheses are relatively new medical devices. The first annuloplasty prosthesis, designed by cardiovascular surgeon Dr. Alain  
20 Carpentier, was introduced in the early 1980's. Several other designs, including one by Professor Carlos Duran, followed shortly thereafter. Annuloplasty prostheses consist of three types: rigid, semi-flexible and flexible. Currently available rigid or flexible  
25 prostheses may be entirely composed of a biocompatible fabric (classified as flexible) such as polyester.

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Alternatively, a prosthesis may constitute a multiple component system composed of a more rigid core such as titanium, polyethylene or silicone, which is then covered by a fabric (classified as rigid or flexible depending on 5 the core material). Some of the prostheses are made radiopaque through use of metal or by impregnating polymers with barium sulfate ( $\text{BaSO}_4$ ).

The Carpentier-Edwards® ring (see, e.g. U.S. Patent No. 5,061,277) is classified as rigid. This 10 prosthesis is kidney shaped with one long curved segment corresponding to the posterior annulus; the ring is open in the portion corresponding to the anterior leaflet. It is constructed of a titanium alloy core with a sewing ring margin that consists of silicone rubber covered with 15 polyester knit fabric. The Medtronic-Duran ring (Duran et al., Circulation (Suppl. I) 78:91-96 (1989)) is classified as flexible and, like the Carpentier ring, is not adjustable after implantation. It is constructed of a radiopaque core of silicone elastomer impregnated with 20 ( $\text{BaSO}_4$ ), and covered by polyester. It is claimed that this prosthesis can adapt to change in the mitral annulus, permitting optimal hemodynamics in diastole while maintaining coaptation and valve integrity in systole. The Puig-Massana Ring (see, e.g. U.S. Patent 25 No. 4,290,151) is a flexible and adjustable prosthesis that is also constructed of a core of silicone elastomer

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impregnated with (BaSO<sub>4</sub>). The adjustability feature is not fully functional since the ring slips under the suture line resulting in equalization of tension around the entire ring. The Carpentier-Edwards Physio™

- 5 Annuloplasty Ring (see, e.g., U.S. Patent No. 5,104,407) is a semi-rigid prosthesis that combines support for valve repair, yet has flexible properties allowing dynamic movement throughout the cardiac cycle. Other prostheses include partial rings (e.g., Cosgrove-  
10 Edwards™, U.S. Patent No. 5,290,300) which are constructed of polyester and are intended to be used only in the posterior mitral annular segment.

The ability of the valve to change shape during the cardiac cycle influences hemodynamic  
15 performance. It has been reported that the mitral annulus dilates 20% to 50% during diastole. Ormiston et al., Circulation 64:113-120 (1981). The hemodynamics seen with flexible prostheses 2 to 3 months following implantation have been reported to be better than that  
20 seen for rigid prostheses. However, by one year post-implantation the hemodynamics are the same for both groups. This may be due to tissue encapsulation of the prosthesis, thereby affecting its flexibility. However, the data do indicate that there may be less post-surgical  
25 morbidity and mortality with flexible prostheses than that seen with rigid prostheses. David, Ann. Thorac.



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Surg. 47:524-528 (1989). Rigid prostheses can prevent the ventricle from working efficiently by restricting annulus motion. In addition, rigid prostheses are more likely to dehiscence than flexible devices. Dehiscence is  
5 due to the normal movement of the mitral valve annulus during systole and diastole and the resultant tension on the suture lines. Cohn, Ann. Thorac. Surg., 45:284-290 (1988). Rigid prostheses also have a higher incidence of systolic anterior motion (SAM) of the mitral valve that  
10 can cause subaortic stenosis.

Suturing techniques for annuloplasty prostheses may vary depending on the design or the physician's preference. The suture may be placed around the prosthesis or passed through a portion of the prosthesis.  
15 Surgeons generally use either interrupted single or mattress sutures, or a continuous running suture similar to that used in prosthetic valve replacement.

An important drawback of all the currently available annuloplasty prostheses is that they are  
20 constructed of nonbiodegradable materials which, as discussed above, eventually are encapsulated by tissue and become rigid. This may lead to a stenotic valve that has suboptimal hemodynamics. Ideally, a bioresorbable annuloplasty prosthesis allows a natural, physiologically  
25 functional annulus to be reformed.

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Summary of the Invention

The invention relates to an annuloplasty prosthesis for use in remodeling a diseased annulus of a natural heart valve, comprising a biocompatible, 5 resorbable member that is sized and shaped to extend about at least a substantial portion of the circumference of the annulus. Following surgical implantation, the member is resorbed at a rate allowing regeneration of reinforcing tissue in the annulus. The member can be 10 adapted to function at the tricuspid, mitral or aortic valve positions of the heart. In one embodiment, the member may be sized and shaped to extend about less than the whole of the circumference of an annulus. Such an "open" or "non-continuous" member has opposed, spaced 15 apart ends, the annular arcuate spacing between the ends being not less than about 1% and not more than about 50% of the whole of the circumference.

The member may comprise a biocompatible, resorbable polymer. The polymer can be composed of, 20 without limitation, dextran, hydroxyethyl starch, gelatin, derivatives of gelatin, polyvinylpyrrolidone, polyvinyl alcohol, poly[N-(2-hydroxypropyl)methacrylamide], polyglycols, polyesters, poly (orthoesters), poly (ester-amides) and 25 polyanhydrides. The polyesters can include, without limitation, poly (hydroxy acids) and copolymers thereof,

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poly ([epsilon]-caprolactone), poly (dimethyl glycolic acid) and poly (hydroxy butyrate). In a preferred embodiment, the polymer is selected from the group consisting of D,L-polylactic acid, L-polylactic acid, 5 glycolic acid and copolymers of D,L-polylactic acid, L-polylactic acid, and glycolic acid.

The member may be manufactured to be of non-uniform rigidity. Preferably, the polymer of the member is invested with one or more biological response 10 modifiers, including without limitation cell adhesion molecules, growth factors and differentiation factors.

The invention also includes a method for treating a patient having a diseased or defective tricuspid valve, comprising providing a resorbable annuloplasty prosthesis 15 adapted for functioning at any one of the tricuspid, mitral or aortic valve positions of the heart, and surgically implanting the prosthesis in the heart of a patient.

#### 20 Brief Description of the Figures

Fig. 1 depicts a "closed" or "continuous" embodiment of the bioresorbable annuloplasty prosthesis of the present invention.

Fig. 2 depicts an "open" or "non-continuous" 25 embodiment of the bioresorbable annuloplasty prosthesis of the present invention.

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Fig. 3 depicts a ring-like annuloplasty prosthesis contoured and adapted for use in aortic valve repair.

Description of the Preferred Embodiments

The invention relates to annuloplasty prostheses used to correct tricuspid, mitral and aortic valve insufficiencies. The resorbable annuloplasty prosthesis of the present invention will allow reinforcement of the annular tissue for the time period necessary to achieve optimal regeneration of a natural annular structure. The regenerated tissue will completely replace the resorbable prosthesis, thereby leaving the recipient with a completely biological and functional annular structure that supports leaflet coaptation and optimal hemodynamics.

A bioresorbable annuloplasty prosthesis generally may be circular in cross section. The annuloplasty prosthesis may be continuous, or may be non-continuous. The shape of the prosthesis generally mimics the shape of the native annulus. The prosthesis can be designed to mimic the structural and functional properties of a healthy annulus. Specifically, the resorbable annuloplasty prosthesis has the following properties:

1. The bioresorbable prosthesis possesses sufficient mechanical properties to maintain coaptation and

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valve competence, but sufficient flexibility to permit good hemodynamics during diastole. The structural or functional properties may vary along the prosthesis to mimic the natural annular structure.

5

2. Prostheses may be manufactured in various sizes and shapes to accommodate the wide variation in annular morphologies.

10

3. The bioresorbable prosthesis degrades at a rate that allows substantially complete regeneration of the host annular structure. The resulting time period to resorption may be on the order of 4 to 6 months.

15

4. Tissue integration may be encouraged with the incorporation of biological response modifiers into the prosthesis. These substances include but are not limited to cell adhesion molecules, growth factors, differentiation factors and cytokines.

20

In addition, heparin or other anticoagulants can be added to the prosthesis if blood compatibility is an issue. X-ray detectable substances can be incorporated into the prosthesis if desired.

25

5. An open cell structure (see below) allows rapid clot stabilization within the prosthesis, facilitating tissue ingrowth. A stable clot facilitates adhesion of the prosthesis to the host

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tissue and prevents peri-valvular leakage.

The main advantage of the bioresorbable annuloplasty prosthesis is that it encourages reinforcement of a diseased annulus with natural tissue rather than with foreign materials. The "naturally" remodeled tissue annulus has advantageous hemodynamic properties during diastole and allows sufficient leaflet coaptation during systole. Endocarditis that could occur during the remodeling phase may be minimized with the use of poly( $\alpha$ -hydroxy) acid bioresorbable polymers due to their ability to induce inflammatory leukocytes' bactericidal function. Devereux, D.F. et al., J. of Surgery, 162:243-246, 1991. Even in the situation in which the surgical implantation must be re-done, there is no pre-existing implant to remove. The resorbable annuloplasty prosthesis is as easy to use and implant as other non-resorbable annuloplasty prostheses. Usually, the prosthesis is not manufactured to have an adjustable circumference, although such adjustability is not excluded from the prosthesis of the present invention.

The concept of a bioresorbable annuloplasty prosthesis that is substantially or completely replaced by functional annular tissue is new. All other annuloplasty prostheses are composed of non-resorbable materials that cause varying degrees of foreign body

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response long term, and which eventually become encapsulated by fibrous tissue. Such encapsulation can adversely affect function.

The resorbable annuloplasty prosthesis has  
5 mechanical properties sufficient to support the valve during implantation and during the post-implant healing period, while allowing the function of the adjacent structures, for example, the aorta, to be retained. Preferably the prosthesis is of sufficient flexibility  
10 such that the native compliance of the adjacent host structures (e.g., chordae tendineae, papillary muscles, aorta) and of the valve commissures is not significantly reduced.

Preferably, the bioresorbable material of the  
15 prosthesis resorbs, post implantation, at a rate that allows good tissue incorporation, but that also results in sufficient resorption within the normal post-operative period, approximately 4 to 6 months. A variety of resorbable, biocompatible materials, for example  
20 polymers, may be employed for manufacture of the prosthesis of the present invention. Homopolymers and copolymers such as those disclosed in U.S. Patent No. 5,412,068, incorporated herein by reference, are appropriate for the resorbable prostheses of the present  
25 invention. Other polymers include without limitation dextran, hydroxyethyl starch, gelatin, derivatives of

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gelatin, polyvinylpyrrolidone, polyvinyl alcohol, poly[N-(2-hydroxypropyl)methacrylamide], polyglycols, polyesters, poly (orthoesters), poly (ester-amides) and polyanhydrides. Preferably the resorbable annuloplasty  
5 prostheses of the present invention are fashioned from polyesters such as poly (hydroxy acids) and copolymers thereof, poly ( $\epsilon$ -caprolactone), poly (dimethyl glycolic acid), or poly (hydroxy butyrate).

Most preferably the prostheses are manufactured of  
10 polymers of D,L-polylactic acid, L-polylactic acid, or glycolic acid, or copolymers of D,L-polylactic acid, L-polylactic acid, and glycolic acid. Such polymers may be manufactured as disclosed, for example, in U.S. Patent No. 5,133,755, incorporated by reference herein.

15 It will be apparent to the ordinary skilled artisan that particular bioresorbable materials may be chosen to fit particular patient needs. For example, polymers may be chosen to be resorbed within the normal 4-6-month interval referenced above, but other polymers  
20 may be chosen to be resorbed within shorter or longer intervals. Variations in selected times to resorption may depend on, for example, the over-all health of the patient, variations in anticipated immune reactions of the patient to the implant, the site of implantation, and  
25 other clinical indicia apparent to the skilled artisan.

Preferably the fabricated resorbable prosthesis



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has an open, interconnected porosity allowing rapid clot stabilization and subsequent tissue ingrowth. The porous resorbable prosthesis may be fabricated using any of a variety of processes known to those of ordinary skill in the art, including a "replamineform" process, a positive replication process or common textile processes.

The replamineform process involves infiltrating a porous, inorganic structure (typically, calcium carbonate) with wax, dissolving the calcium carbonate, adding the appropriate monomer or mixture of monomers, polymerizing the monomers, and finally increasing the temperature to withdraw the wax. See, for example, Hiratzka et al., Arch. Surgery 114: 698-702 (1979), incorporated herein by reference. This process yields a positive copy of the porous, inorganic structure. Negative copies or casts of the porous inorganic structure may be made by filling the pores with a selected polymer, then dissolving the inorganic matrix (e.g., calcium carbonate) as a final step. What remains following completion of either the positive- or negative-cast steps of the replamineform process is a polymer with defined porosity.

A positive replication process is disclosed in, for example, Jamshidi et al., Resorbable Structured Porous Materials in the Healing Process of Hard Tissue Defects, ASAIO 34: 755-60 (1988); incorporated herein by

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reference. In principle, a positive replication process is very similar to the replamineform process.

In a further alternative embodiment, porosity can also be introduced into the prosthesis by mixing the  
5 polymer with particles of a specific size range (e.g., 20 to 300 micron diameters), then dissolving those particles during a final stage of the fabrication process. For example, sodium chloride crystals may be incorporated into a polymer or copolymer by adding crystals of the  
10 salt to a solution of dissolved polymer. After evaporating the solvent, annealing the polymer or copolymer by heating, and cooling at controlled rates, the sodium chloride crystals may be leached out. This leaves a porous polymer matrix. Porosity and pore size  
15 may be controlled by varying the concentration and size of the crystals. See, for example, Hubbell and Langer, Chem. & Engineering News, March 13, 1995, pages 47-50, incorporated herein by reference.

The open porosity of the above-described  
20 resorbable prostheses provides a scaffold for cellular ingrowth. To facilitate ingrowth of host or other cells after implantation, a variety of biological response modifiers may be incorporated into the structure of the resorbable prosthesis. Biological response modifier  
25 molecules may be covalently or non-covalently coupled to the various internal and external surfaces defining the

porosity of the resorbable prosthesis, or may be incorporated directly into the resorbable material during, for example, the polymerization process. In the latter case, the biological response modifier is slowly released as the prosthesis is resorbed.

Appropriate biological response modifiers may include, for example, cell adhesion molecules, cytokines including growth factors, differentiation factors, and antimicrobials. Cell adhesion molecules (CAM) may be incorporated into the resorbable prosthesis in order to stimulate cell attachment, which is critical for normal cell function. Various CAM useful for incorporation include without limitation fibronectin, vitronectin, fibrinogen, collagen and laminin. See, e.g., Beck et al., J. FASEB 4: 148-160 (1990); Ruoslahti et al., Science 238: 491-97 (1987). The cell attachment activity has been isolated to specific amino acids sequences (expressed herein with standard single-letter code), for example RGD in the case of fibronectin, fibrinogen, collagen, osteopontin and others, REDV from fibronectin and YIGSR from laminin. Hubbell et al., Bio/Technology 9: 586-72 (1991); Humphries et al., J. Cell Biol. 103: 2637-47 (1986); Graf et al., Cell 48: 989-96 (1987). Other examples of cell attachment domains include the heparin-binding domains of fibronectin, KQAGDV and GPRP-containing peptides of fibrinogen and EILDV-containing

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peptides of fibronectin. Hynes et al., Cell 69: 11-25 (1992); Loike et al., Proc. Natl. Acad. Sci. USA 88: 1044-48 (1991). Thus, any cell attachment peptide-containing molecules functional as CAM for the cells seeded onto or migrating into the resorbable prosthesis may be incorporated into the prosthesis structure during or after fabrication.

Cellular ingrowth may be further facilitated through use of growth factors, including without limitation the fibroblast growth factors including acidic (FGF 1), basic (FGF 2) and FGF 3 through 9, platelet-derived growth factors including PDGF, PDGF-AA, PDGF-BB and PDGF-AB, transforming growth factors ( $\beta 1 - \beta 5$ ), epidermal growth factors including heparin-binding EGF, transforming growth factor  $\alpha$  and other members of the epidermal growth factor family, the insulin-like growth factors I and II, platelet-derived endothelial cell growth factor and vascular endothelial growth factor. These factors have been shown to stimulate cellular migration (useful for attracting the appropriate cell population(s) into the prosthesis), proliferation (cell replication) and protein synthesis (required for production of extracellular matrix as the newly indwelling cells remodel the resorbing structure of the prosthesis). Albumin may be added to a particular growth factor to increase its effectiveness. Murray et al.,

Cancer Drug Delivery 1: 119 (1984).

Other biological response modifiers that may be incorporated into the resorbable annuloplasty prosthesis of the present invention include without limitation

5 polysaccharides, mucopolysaccharides, glycoproteins, and glycosaminoglycans such as hyaluronic acid, chondroitin, chondroitin 4-sulfate, dermatan sulfate, keratan sulfate, heparin, heparan sulfate, alginate, poly-D-lysine, laminin and collagen types I, III and IV. It will be

10 apparent to the ordinary skilled artisan that variations in individual biological response modifiers or combinations of biological response modifiers may be employed to suit the requirements of particular cell types, prosthesis materials, prosthesis configurations,

15 sites of implantation and patient needs.

As described above, the bioresorbable prosthesis may be fabricated to have a structure conducive to formation of a stabilized blood clot after implantation. Such prostheses may have relatively high porosity, i.e.,

20 relatively high internal surface area (see above).

Alternatively, the stabilized clot may be induced to form by inclusion of chemicals, e.g., coagulants, into the prosthesis structure as described above. Inducing a stabilized clot layer to form on the surface upon

25 implantation facilitates cell ingrowth and healing, with the clot layer potentially functioning as a provisional

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matrix for healing, comparable to that occurring during normal vessel repair. Van Der Lei et al., Int. Angiol. 10: 202-08 (1991), for example, reported on the poor healing of expanded polytetrafluoroethylene prostheses in general, but also reported success in encouraging complete healing by inducing a clot layer to form on the graft surface upon implantation.

Referring now to the Figures, a resorbable annuloplasty prosthesis may be fashioned to have a generally oval shape similar to that of the native tissue annulus. For example, the prosthesis depicted in Figure 1 is designed to conform to the shape of the base of the mitral valve, and has substantially the shape of a closed, continuous ring 2. Closed ring 2 may be circular, oval or, as shown, slightly straightened at 4 over a length of its periphery. Substantially straight portion 4 corresponds to the curvature of the anterior leaflet, and the opposite, complementary zone 6 corresponds to the curvature of the posterior leaflet.

The prosthesis has in its plane an axis of symmetry, with its largest dimensions, along this axis and along a perpendicular axis, being generally between about 15 and 30 mm and about 15 and 40 mm respectively. Any given portion of the prosthesis may be generally circular in cross section, or may be oval or flattened in cross section.

In an alternative embodiment as depicted in Figure 2, the prosthesis may be in the form of an open, non-continuous ring 8 that is slightly straightened over a length of the periphery. A non-continuous design may be desired for hemodynamic performance and implant considerations. This part-annular-shaped prosthesis is open over a length generally between about 1% and 50% of the total annular shape. The free ends 10 and 12 of the open ring 8 are rounded or otherwise shaped so as not to damage the tissue in which they are disposed after implantation.

It will be appreciated by the ordinary skilled artisan that the prosthesis of the present invention can be sized and shaped to any useful configuration appropriate to the mitral, tricuspid or aortic valve of an individual patient. For example, the prosthesis may be shaped generally as depicted in Figure 3 so as to follow the contours of the commissures of the aortic valve, i.e., to be adapted to the trifoliate form of the aortic valvular orifice. In an alternative embodiment, an aortic valve annuloplasty prosthesis can be manufactured to include a sleeve or collar extending upward (with respect to the orientation depicted in Figure 3), from along all or a substantial portion of the contour length. In this orientation, the sleeve or collar extends upward from the contoured ring-like

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prosthesis into the aortic root or complex. The sleeve or collar thereby facilitates attachment to and additional remodeling of the aortic complex above the commissures.

- 5           The resorbable material of the annuloplasty prosthesis preferably is flexible, with the flexibility selected and manufactured to approximate that of the native annulus and its supporting structure. As desired, the rigidity of the prosthesis (reflective of
- 10 flexibility) may vary from one point to another on the prosthesis, i.e., the prosthesis may be of non-uniform rigidity. For example, more flexibility may be desired in the posterior part of the mitral valve annulus than the anterior part. This can be accomplished by
- 15 controlling porosity of the matrix. In this manner, rigidity of the resorbable polymeric prosthesis material may be made to vary continuously from one region of the prosthesis to another region, or may vary in multiple step-wise increments from one region to another.
- 20           Any sutures used for attachment of the resorbable annuloplasty prosthesis to a patient may be bioresorbable. Preferably the resorption rate of the sutures is similar to that of the prosthesis.

A resorbable annuloplasty prosthesis of the

25 present invention is implantable with a variety of surgical techniques appropriate to the configuration of



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the valvular tissue (e.g., annulus) and prosthesis and to the site of implantation. These surgical procedures will be apparent to the ordinary skilled artisan, and may include without limitation techniques such as disclosed in U.S. Patent No.'s 3,656,185 and 4,042,979, incorporated herein by reference. Annuloplasty surgical procedures such as may be used with the annuloplasty prostheses of the present invention are also disclosed in Murphy et al., Ann. Thorac. Surg. 43: 52-8 (1987) and in Gorton et al., Ann. Thorac. Surg. 55: 860-3 (1993).

Generally, a series of interrupted or continuous sutures is placed around the tissue annulus. The annuloplasty prosthesis is then parachuted down the sutures and tied in place. Following this, the cardiovascular incision (e.g., aortotomy) is then closed and the heart restarted.

With the resorbable annuloplasty prosthesis of the present invention, cross-clamp times for implantation will approximate those required with present annuloplasty rings, in which the prosthesis consists of non-resorbable materials.

The foregoing detailed description has been provided for a better understanding of the invention only and no unnecessary limitation should be understood therefrom as some modifications will be apparent to those skilled in the art without deviating from the spirit and scope of the appended claims.

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What is claimed is:

1. An annuloplasty prosthesis for use in remodeling a diseased annulus of a natural heart valve, comprising a biocompatible, resorbable member that is sized and shaped to extend about at least a substantial portion of the circumference of said annulus, wherein, following surgical implantation, said member is resorbed at a rate allowing regeneration of reinforcing tissue in said annulus.
2. The annuloplasty prosthesis of claim 1, wherein said member is adapted to function at the tricuspid valve position of the heart.
3. The annuloplasty prosthesis of claim 1, wherein said prosthesis is adapted to function at the mitral valve position of the heart.
4. The annuloplasty prosthesis of claim 1, wherein said prosthesis is adapted to function at the aortic valve position of the heart.
5. The annuloplasty prosthesis of claim 4, wherein said member is shaped to follow the contours of the aortic valve commissures.

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6. The annuloplasty prosthesis of claim 5, wherein said member further includes a collar adapted for attachment to the aortic complex above said commissures.

7. The annuloplasty prosthesis of claim 1, wherein  
5 said member comprises a biocompatible, resorbable polymer.

8. The annuloplasty prosthesis of claim 7, wherein said polymer is selected from the group consisting of dextran, hydroxyethyl starch, gelatin, derivatives of  
10 gelatin, polyvinylpyrrolidone, polyvinyl alcohol, poly[N-(2-hydroxypropyl)methacrylamide], polyglycols, polyesters, poly (orthoesters), poly (ester-amides) and polyanhydrides.

9. The annuloplasty prosthesis of claim 8, wherein  
15 said polyesters are selected from the group consisting of poly (hydroxy acids) and copolymers thereof, poly ([epsilon]-caprolactone), poly (dimethyl glycolic acid) and poly (hydroxy butyrate).

10. The annuloplasty prosthesis of claim 7, wherein  
20 said polymer is selected from the group consisting of D,L-polylactic acid, L-polylactic acid, glycolic acid and copolymers of D,L-polylactic acid, L-polylactic acid, and

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glycolic acid.

11. The annuloplasty prosthesis of claim 1, wherein said member is of non-uniform rigidity.
12. The annuloplasty prosthesis of claim 7, wherein  
5 said polymer is invested with one or more biological response modifiers.
13. The annuloplasty prosthesis of claim 12, wherein said one or more biological response modifiers are selected from the group consisting of cell adhesion  
10 molecules, growth factors and differentiation factors.
14. A method for treating a patient having a diseased or defective tricuspid valve, comprising:
  - a) providing the annuloplasty prosthesis of claim 2; and
  - 15 b) surgically implanting said annuloplasty prosthesis in the heart of said patient.
15. A method for treating a patient having a diseased or defective mitral valve, comprising:
  - a) providing the annuloplasty prosthesis of claim  
20 3; and
  - b) surgically implanting said annuloplasty

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prosthesis in the heart of said patient.

16. A method for treating a patient having a diseased or defective aortic valve, comprising:

a) providing the annuloplasty prosthesis of claim

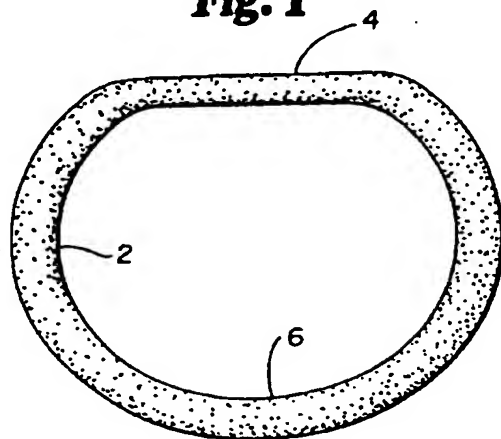
5 4; and

b) surgically implanting said annuloplasty prosthesis in the heart of said patient.

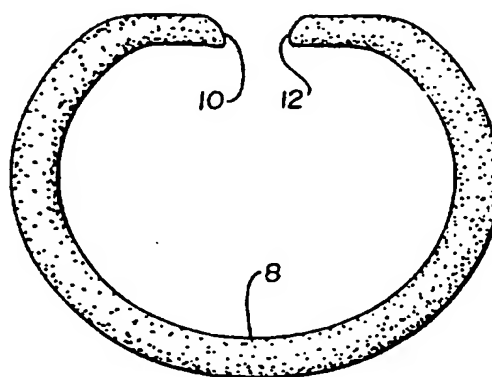
17. The annuloplasty prosthesis of claim 1, wherein said member is sized and shaped to extend about less than  
10 the whole of said circumference, said member having opposed, spaced apart ends, the annular arcuate spacing between said ends being not less than about 1% and not more than about 50% of the whole of said circumference.

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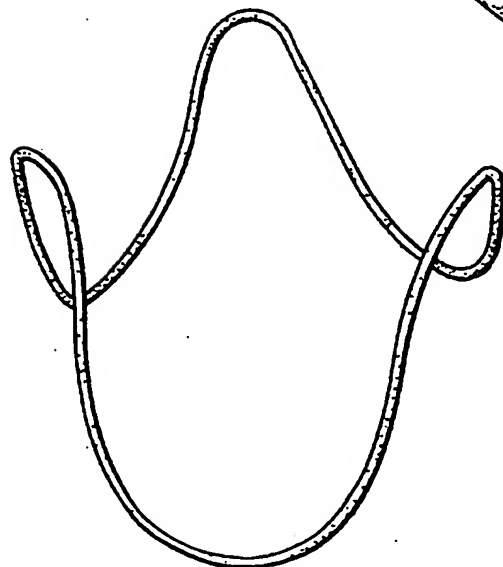
**Fig. 1**



**Fig. 2**



**Fig. 3**



# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 96/17886

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 A61F2/24 A61L31/00 A61B17/11

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 A61F A61L A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 594 148 A (UNITED STATES SURGICAL CORPORATION) 27 April 1994	1-10, 12, 13
Y	see column 1, line 48 - line 55 see column 3, line 54 - column 4, line 7	11, 17
Y	WO 95 03757 A (SEGUIN) 9 February 1995 see abstract; figure 1	11
Y	EP 0 338 994 A (MOREA) 25 October 1989 see figure 1	17
A	US 3 620 218 A (AMERICAN CYANAMID COMPANY) 16 November 1971	

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

### \* Special categories of cited documents:

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Date of the actual completion of the international search

18 February 1997

Date of mailing of the international search report

25.02.97

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Steenbakker, J

# INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 96/17886

## Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☒ Claims Nos.: 14-16  
because they relate to subject matter not required to be searched by this Authority, namely:  
PCT Rule 39.1 (1v)
2. ☐ Claims Nos.:  
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☐ No protest accompanied the payment of additional search fees.



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